



› CONTINUOUS SOLVENT-FREE  
EXTRUSION OF PROPELLANT  
FOR 35 MM CALIBRE  
AMMUNITION

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# OVERVIEW

- › Introduction
- › Approach
- › Propellant composition
- › Rheological modelling and closed vessel testing
- › Propellant grain geometry
- › Preliminary propellant manufacturing and testing
- › Processing with a 30mm co-rotating twin screw extruder
- › Propellant characterization
- › Firing tests
- › Conclusions

# INTRODUCTION

- › Aim of the project: evaluation of new 35 mm calibre ammunition performance
- › In-house testing (TNO Laboratory for Ballistic Research)
  
- › Previously manufactured DB for 35 mm:
  - › DB propellant composition
  - › 45 mm continuous co-rotating twin-screw extruder
  - › 10 wt% solvent
  
- › New DB propellant with equal performance
  - › Comparable composition based on JA-2 replacement
  - › Solvent-free
  - › 30 mm continuous co-rotating twin-screw extruder

# INTRODUCTION

› Current 35 mm ammunition

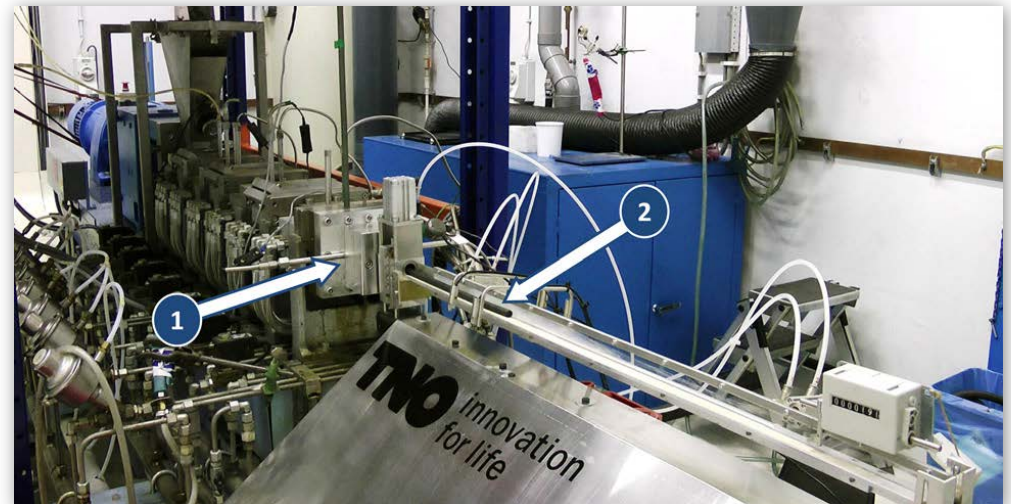


	Projectile weight [kg]	Projectile velocity [m/s]	Propellant weight [kg]	Kinetic energy [kJ]
HE	0.550	1180	0.340	383
FAPDS	0.400	1400	0.375	392
KETF	0.750	1050	0.340	413

# INTRODUCTION



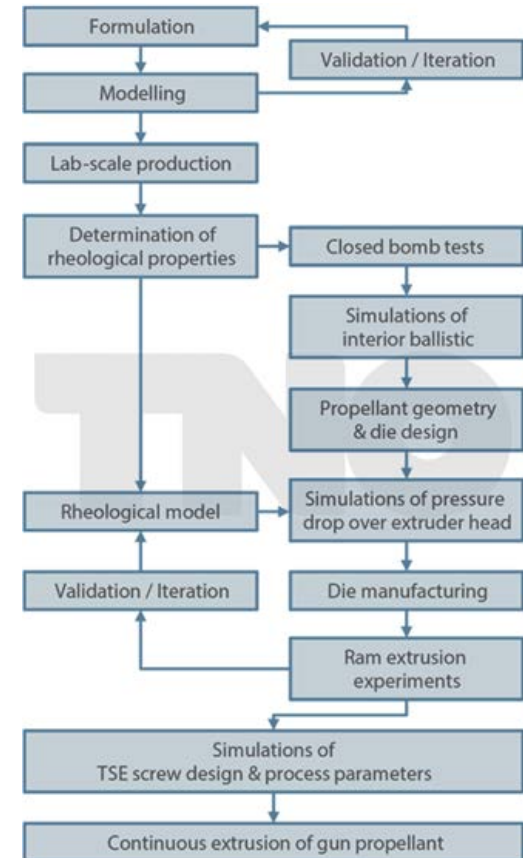
- › Previous work ARDEC/TNO:  
*'Definition of a JA-2 Equivalent Propellant to be Produced by Continuous Solventless Extrusion'*,  
Journal of Applied Mechanics, May 2013
- › 120 mm calibre
- › Propellant grain:
  - › Shape: 19-perf
  - › Diameter: 11.6 mm
- › Produced with 45 mm co-rotating twin-screw extruder (TSE)
  - › 10 – 15 kg/h
  - › Single die



1: extruder head  
2: extruded propellant strand

# APPROACH

- › TNO propellant development approach
- › Thermodynamic-, burning-, and rheological properties known from 120 mm development
- › IB simulations
  - › Small grain diameter required: ~ 5 mm
  - › Development of new die design
- › Ram extrusion experiments to validate burning properties (small scale: < 1 kg)
- › Determination of TSE screw design and process parameters
- › Continuous extrusion batch

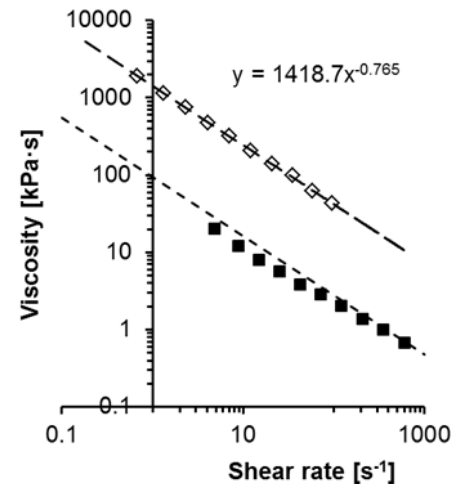


# PROPELLANT COMPOSITION

- › JA-2 equivalent composition
- › Slightly higher content of blasting oils (less than some German tank propellants)
- › Tuning mechanical properties (viscosity; flow behaviour in extruder) by addition of green plasticizer
- › Non-energetic plasticizer reduces flame temperature
  - › Force ~1100 J/g
  - › Flame temperature ~3000 K

# RHEOLOGICAL CHARACTERIZATION

- › Safe TSE operation requires reliable prediction of:
  - › Pressure drop over extruder head and die
  - › Temperatures and pressures along extruder
  
- › Flow of propellant paste through a die is characterized by using a double barrel capillary rheometer
  - › Shear viscosity
  - › Extensional viscosity



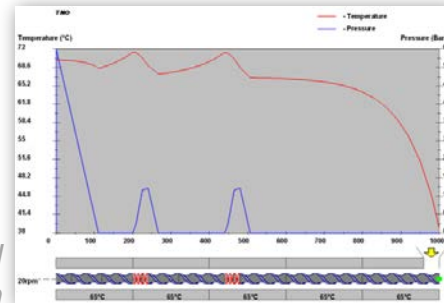
- ◇ Extensional viscosity
- Shear viscosity
- Model fit shear viscosity
- Power law extensional visc.



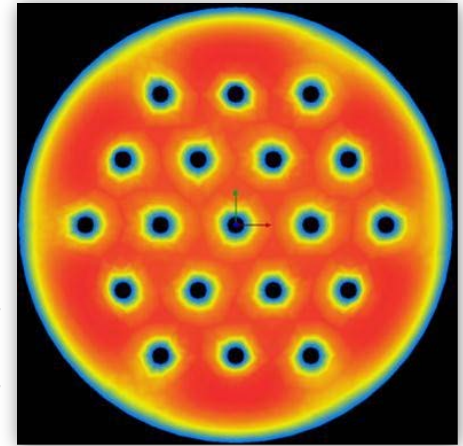
# RHEOLOGICAL MODELLING

- › Pressure drop over die: commercially available 2D-FEM simulation software
- › Extruder head: conical entry part and capillary part of the die (determining final propellant shape; cylindrical, slotted, hexagonal, rosette)
- › TSE screw configuration and process parameters determined by commercially available software

*TSE internal conditions for typical screw configuration*



*Flow pattern in die (red: highest paste velocity, blue: lowest velocity)*

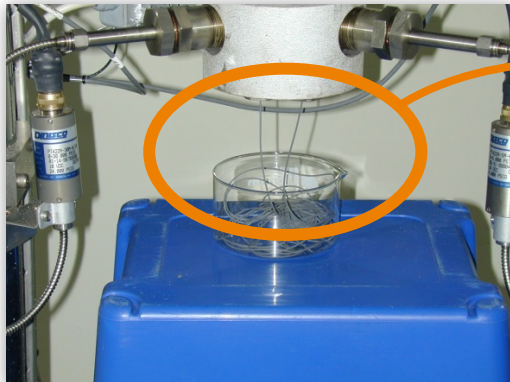


*TSE screws with transport, compacting and kneading elements*

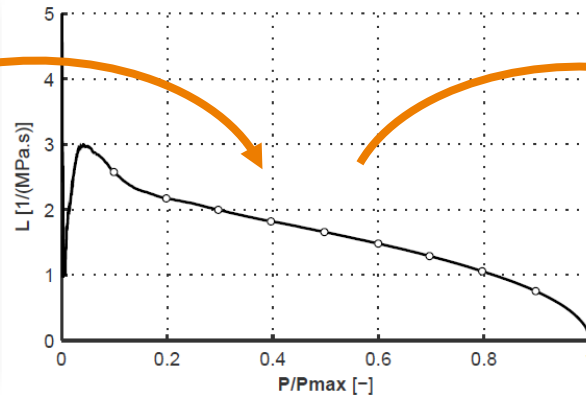


# PROPELLANT GRAIN GEOMETRY

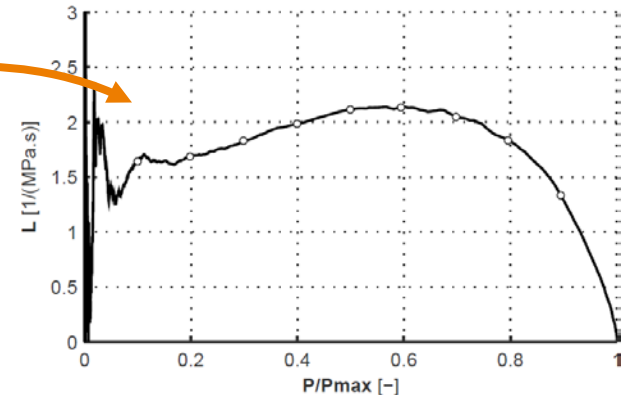
- › Cylindrical 19-perf grain geometry
- › Propellant burn rate determined from closed vessel tests with non-perforated strands (from rheometer)
- › Websize 19-perf grains determined by IB simulations



Non-perf strand

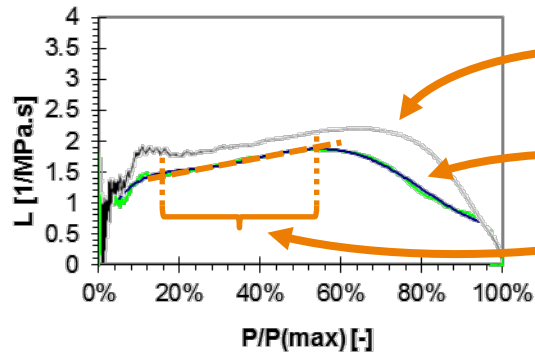


19-perf grain



# PRELIMINARY PROPELLANT

- › Die manufacturing
- › Validation pressure drop by small scale ram extrusion (< 1 kg)
- › Closed bomb testing



Previous batch (produced with 10 wt% solvent)

$$L_{av} = 2.05 \text{ MPa}^{-1} \text{ s}^{-1}$$

Test batch (unequal inner and outer websizes)

Data used for calculation of burn rate and correction of grain geometry

- › Propellant grain geometry optimization / die adjustment (high progressivity = equal websizes)

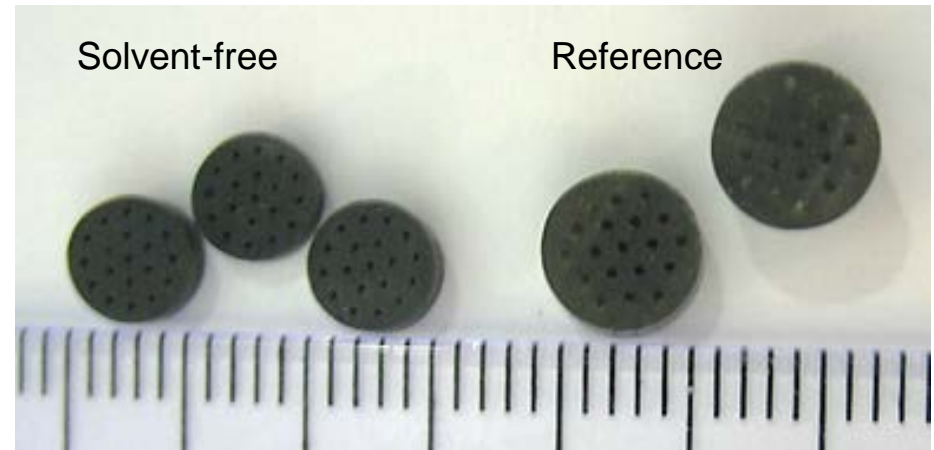
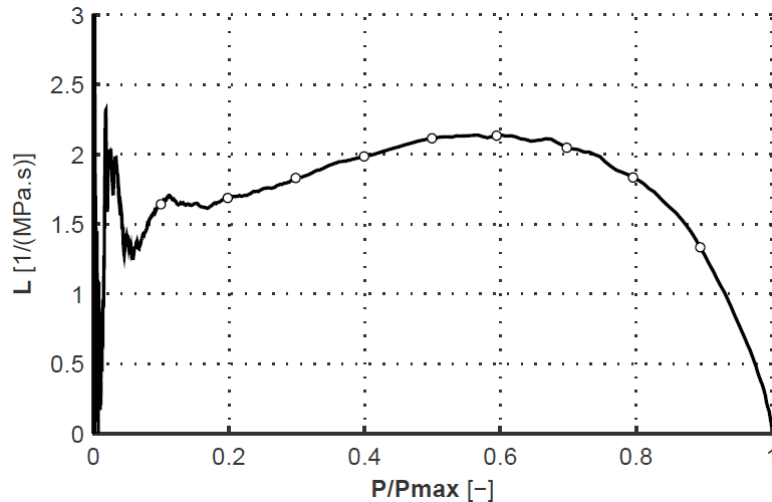
# PROCESSING WITH A 30 MM CO-ROTATING TWIN SCREW EXTRUDER (TSE)



# CHARACTERIZATION OF THE EXTRUDED PROPELLANT

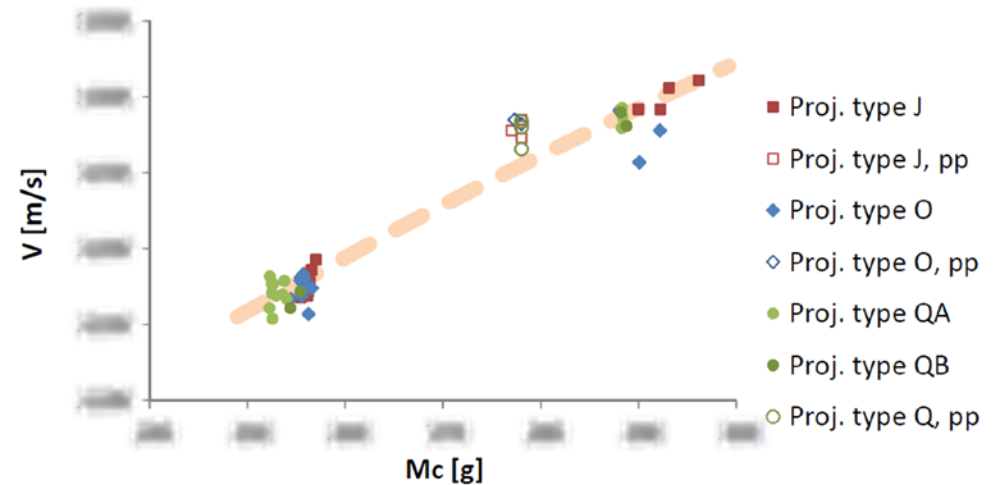
- › Dynamic vivacity:  $L_{(0.3...0.7)} = 2.03 \text{ MPa}^{-1}\text{s}^{-1}$   
Expected:  $L_{(0.3...0.7)} = 2.05 \text{ MPa}^{-1}\text{s}^{-1}$

- › Diameter: 5.1 mm
- › Websize: 0.6 mm
- › Perf. diameter: 0.3 mm



# FIRING TESTS

- › Various projectile types
- › Small variations in projectile mass ( $M_c$ )
- › Equal performance as previous propellant batch ('pp'; manufactured using solvent)
- › Larger dispersion at low charge mass



# CONCLUSIONS

- › The composition and grain geometry of a DB propellant were determined by interior ballistic calculations.
- › Subsequently, the conditions for the manufacturing of this propellant were determined using rheological properties of the propellant paste.
- › The double base propellant was successfully manufactured by solvent-free extrusion using a 30mm co-rotating twin screw extruder.
- › The obtained extrusion conditions were in good agreement with simulations.
- › The propellant dimensions and density were very close to the theoretically expected values.
- › Burn properties and gun performance equal to those of previous propellant batch produced using solvent.



› THANK YOU FOR YOUR  
ATTENTION

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