

The Trouble with TNT Equivalence

Paper: 11770

Presented by

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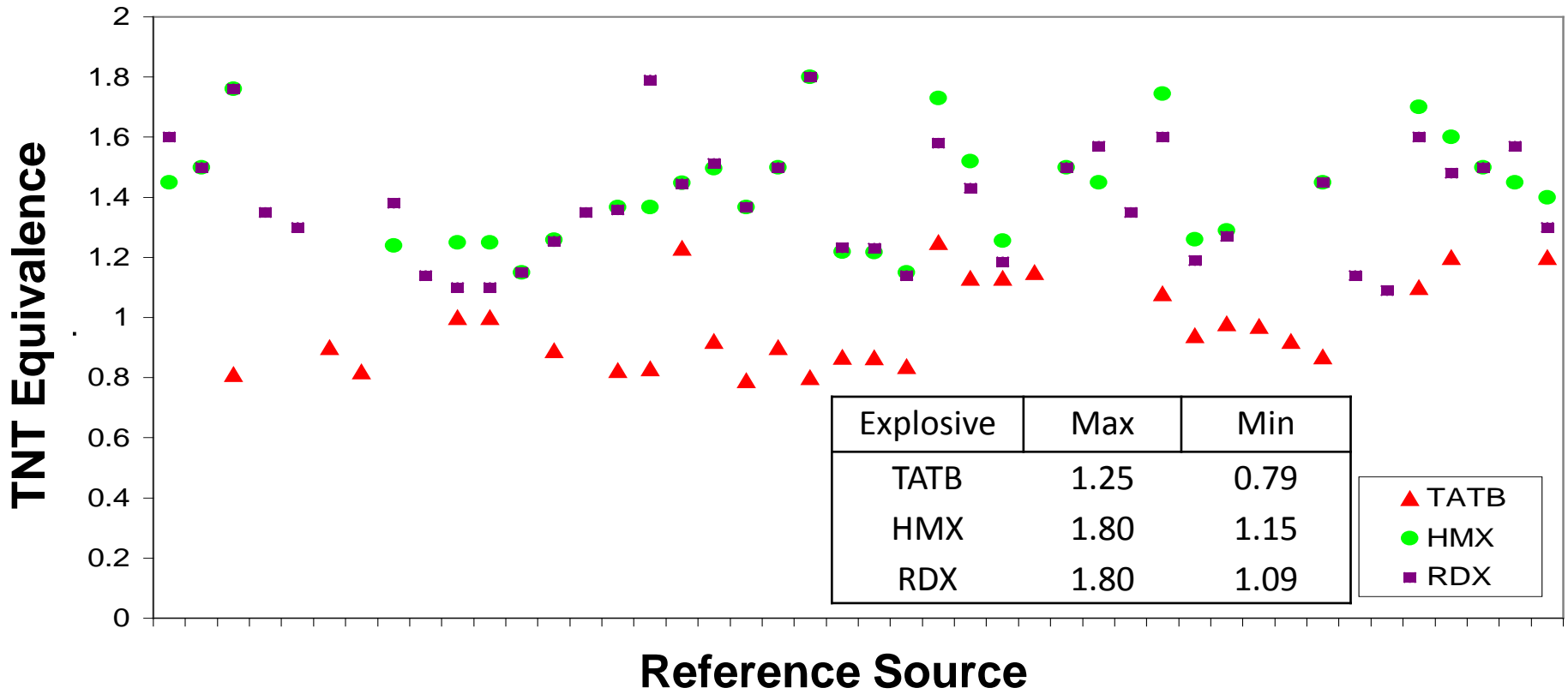


Outline

- The big problem with TNT Equivalence
 - Often used to compare explosives performance
 - Many models use TNT as the baseline explosive
 - 1 kg RDX = 1.6 kg TNT, so giving RDX an Equivalence of 1.6
 - 20% to 30% typical error, 50% has been found
- Scaling Laws
 - Scaled Distance, Scaled Impulse
- Trials techniques will not be discussed here -> see paper
- Theoretical Methods for TNT Equivalence
 - Secondary combustion / Aluminised explosives not covered
- Theoretical fit to trials data
 - Error Analysis
- Conclusions

The Problem

Figure 1. Variation in TNT equivalency of three high explosives TATB, HMX & RDX (from a number of different techniques and sources)



(from Cheesman)

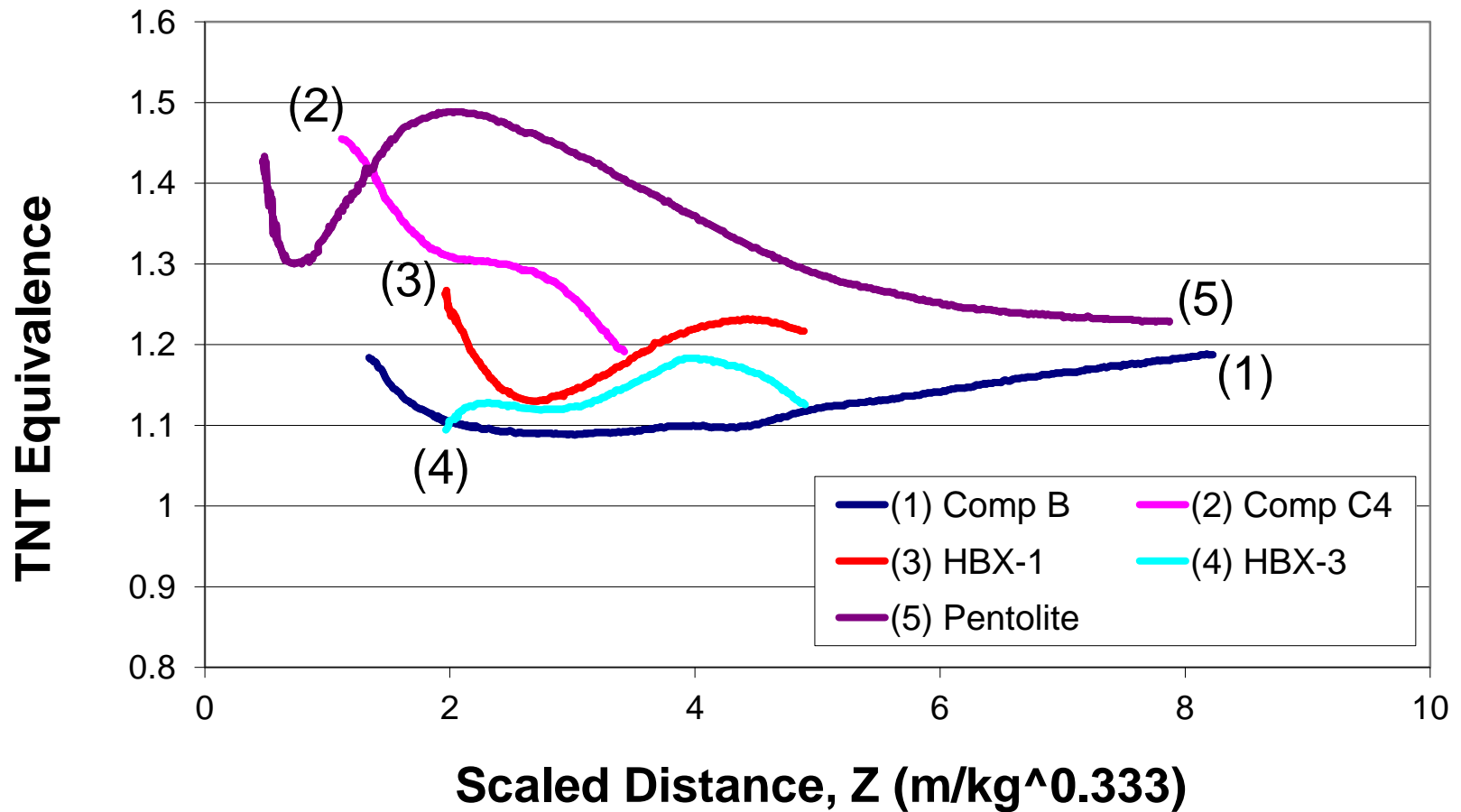
Scaling Laws

- Blast wave scaling laws are often called 'Cube root scaling'
 - Hopkinson (1915) & Crazz (1926)
- Charge performance is a function of Scaled Distance (Z)
- Both peak overpressure & Scaled Impulse are directly related to Scaled Distance

$$\text{Scaled Distance (Z)} = \text{Range} / \text{Charge mass}^{1/3}$$

$$\text{Scaled Impulse} = \text{Impulse} / \text{Charge mass}^{1/3}$$

Figure 2. Variation of TNT Equivalence with Scaled Distance by Cooper



(from Air Blast Calculations and trials by Swisdak)

Figure 3. TNT Equivalence for Peak Positive Incident Pressure
(from UFC 3-340-02 data)

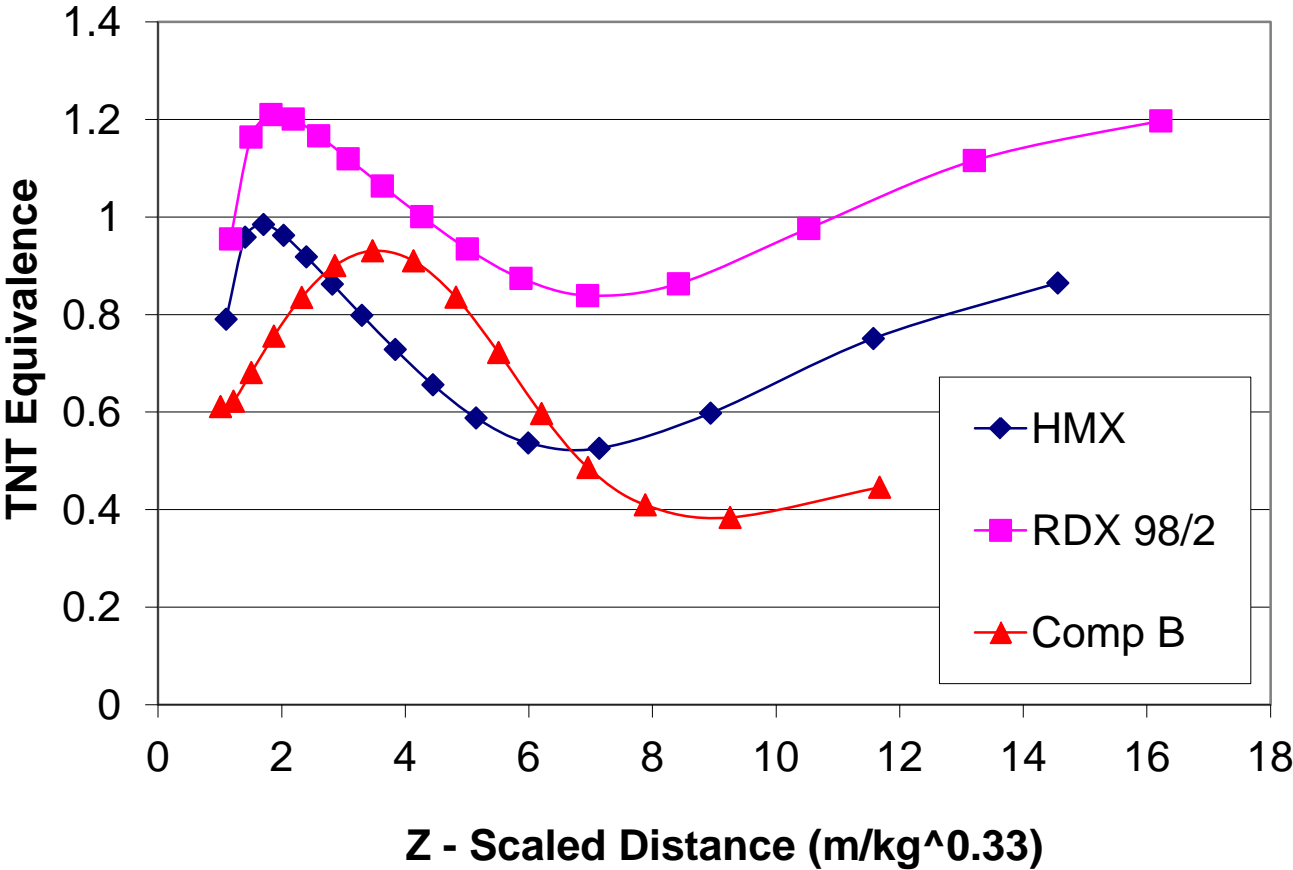


Figure 4. TNT Equivalence for Peak Positive Incident Pressure
(from UFC 3-340-02 data)

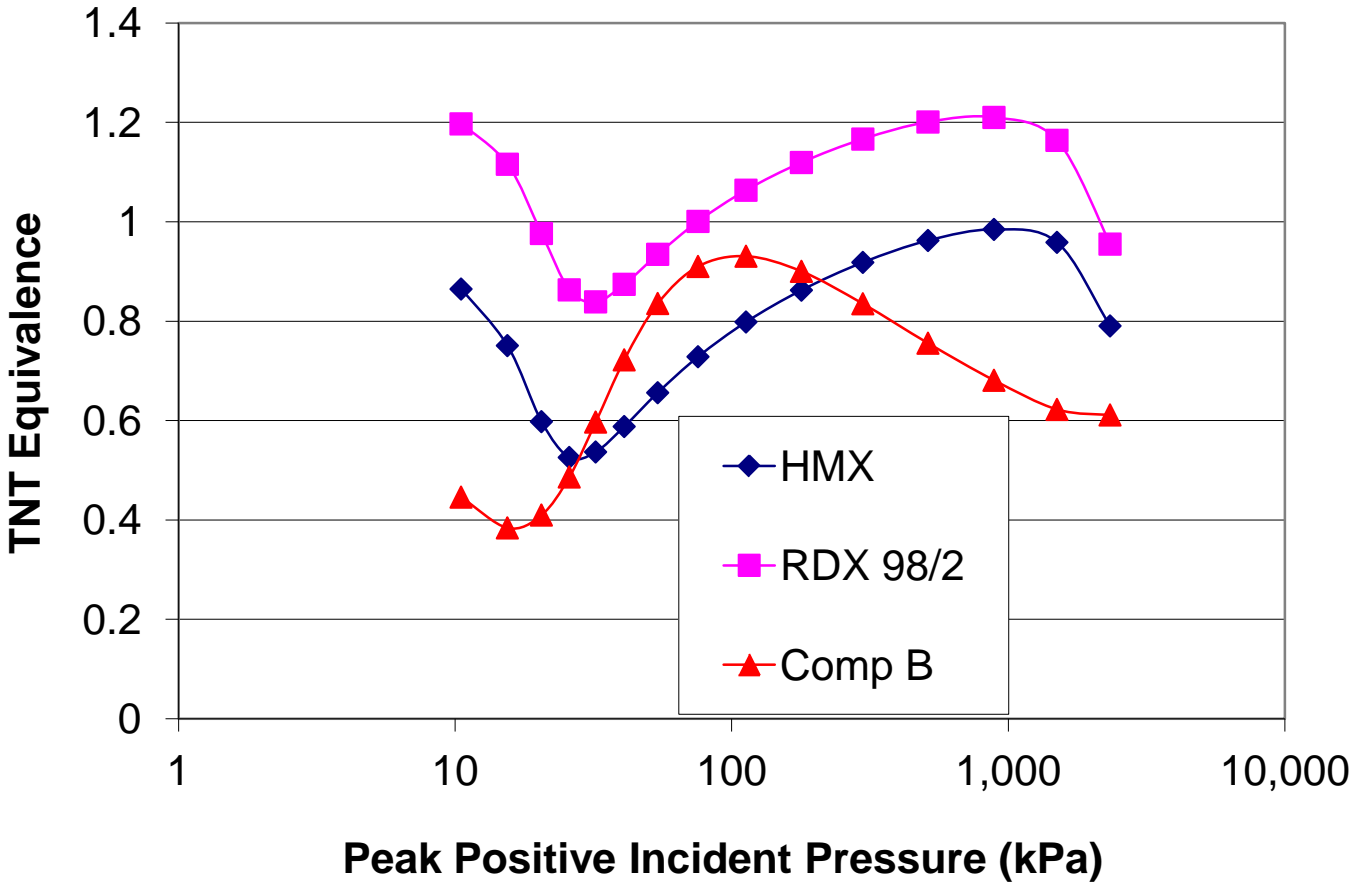


Figure 5. TNT Equivalence for Impulse
(from UFC 3-340-02 data)

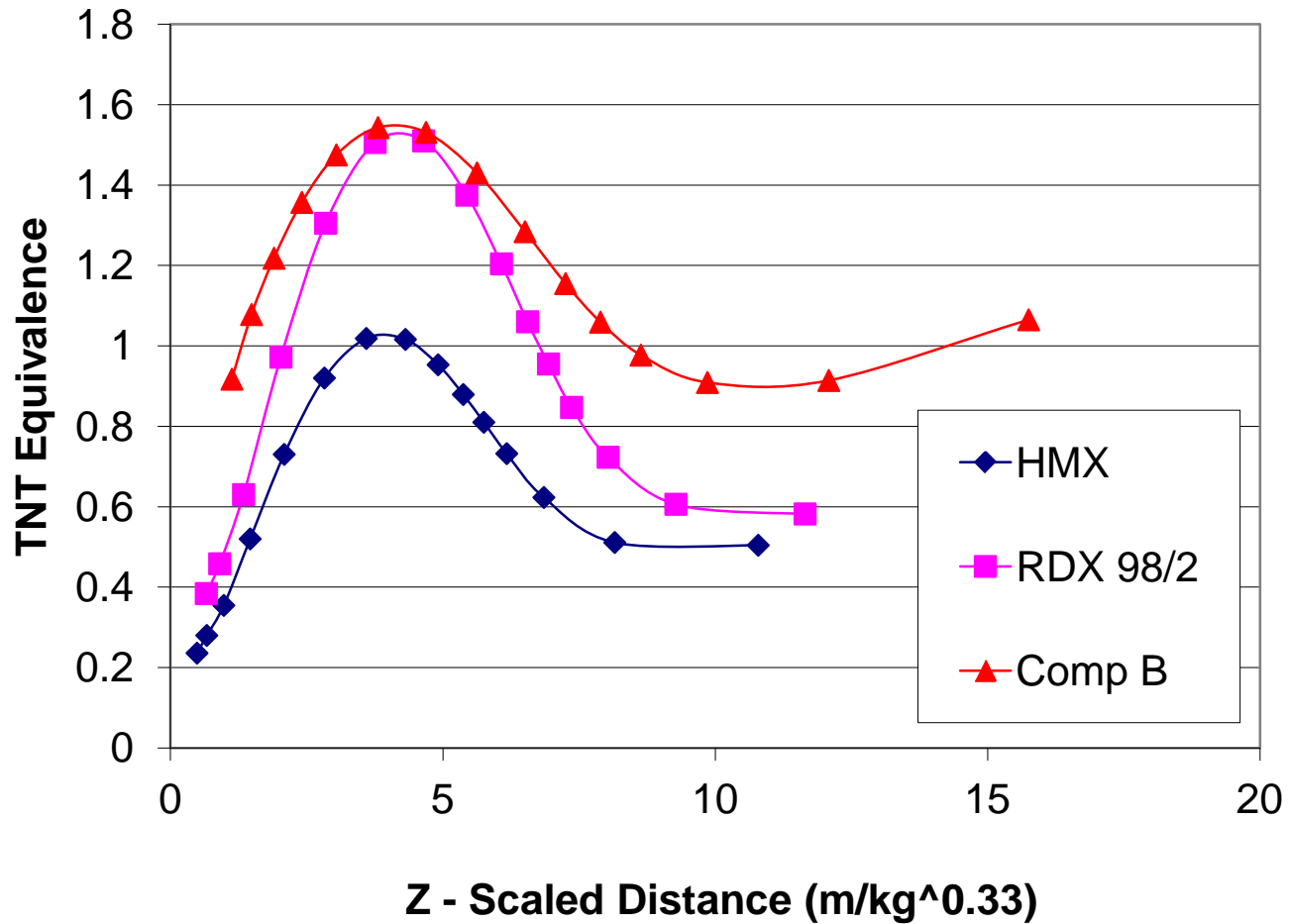


Figure 6. TNT Equivalence for Impulse
(from UFC 3-340-02 data)

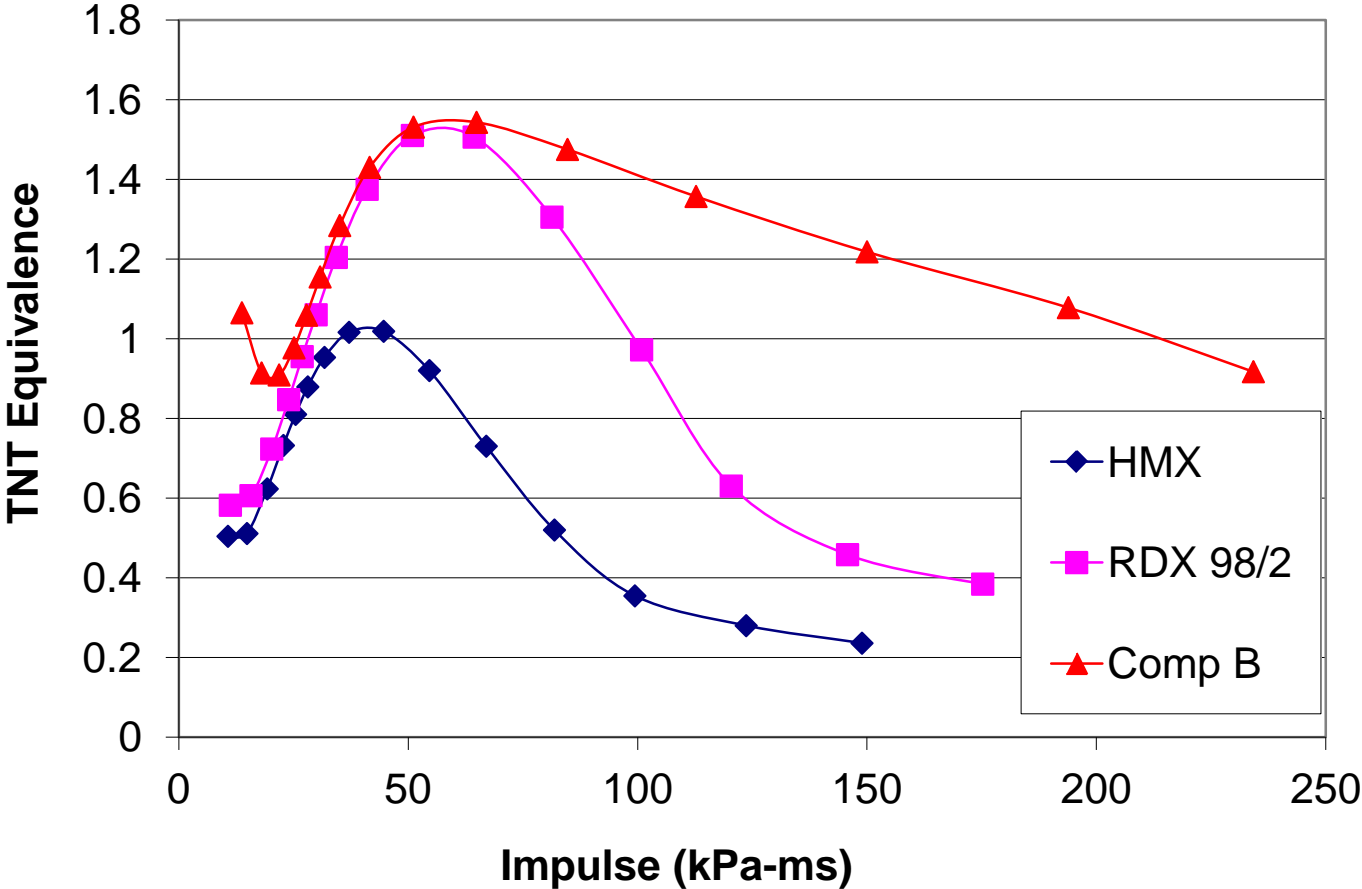


Table II. TNT Equivalence from UFC 3-340-02 Data

(from Figures 3 – 6)

Explosive	TNT Equivalence (%)	
	Peak Incident Pressure	Peak Incident Impulse
HMX	99	102
RDX 98/2	121	151
Comp B	93	154

Theoretical Methods for TNT Equivalence (1 of 3)

- Berthelot Method (1892)

- TNT Equivalent (%) = $840 \cdot \Delta n \cdot (-\Delta H_R^\circ) / \text{Molwt}_{\text{EXP}}^2$

Where:

Δn – Number of moles of gases / mol of explosive

ΔH_R° – Heat of Detonation (kJ/mol)

$\text{Molwt}_{\text{EXP}}$ – Molecular weight of the Explosive (g/mol)

- Cooper Method (D^2)

- TNT Equivalence = $D^2_{\text{EXP}} / D^2_{\text{TNT}}$

Where:

D – Detonation Velocity (m/s)

Theoretical Methods for TNT Equivalence (2 of 3)

- Hydrodynamic Work (E)

$$E = \int_{P_{CJ}}^{P_{AMB}} P(V)_S \cdot dV = 0.36075 \cdot P_{CJ} / \rho_0^{0.96}$$

Where:

P_{CJ} – Chapman-Jouguet (CJ) Detonation Pressure (Pa)

ρ_0 – Density of unreacted explosive (kg/m³)

- Power Index (PI) – related to Explosive Power (EP) = $Q_{EXP} \cdot V_{EXP} \cdot R / (V_{MOL} \cdot C)$

$$\text{Power Index} = Q_{EXP} \cdot V_{EXP} / Q_{TNT} \cdot V_{TNT}$$

Where:

C – Mean Heat capacity of gases from detonation to stp (J/kg/K)

Q_{EXP} – Heat of Detonation of explosive for comparison (J/kg)

Q_{TNT} – Heat of Detonation of TNT (J/kg)

V_{EXP} – Volume of gases at stp / Mass of explosive for comparison (m³/kg)

$V_{MOL} = 22.4$ – Molar volume of gas at stp (m³/mol)

V_{TNT} – Volume of gases at stp / Mass of TNT (m³/kg)

Theoretical Methods for TNT Equivalence (3 of 3)

- Heat of Detonation (Q) – the TM / UFC Standard

- TNT Equivalence (by Q) = Q_{EXP} / Q_{TNT}

Where:

Q_{EXP} – Heat of Detonation of explosive for comparison (J/kg)

Q_{TNT} – Heat of Detonation of TNT (J/kg)

- Heat of Detonation (Q) – Updated method in paper

- TNT Equivalence (by Q) = $Q_{EXP} / (Q_{TNT} (1 - d) + m \cdot Q_{EXP})$

Where:

d – Line intercept = 0.76862

m – Line gradient = 0.7341

Figure 7. TNT Equivalence Difference for Heat (Q)

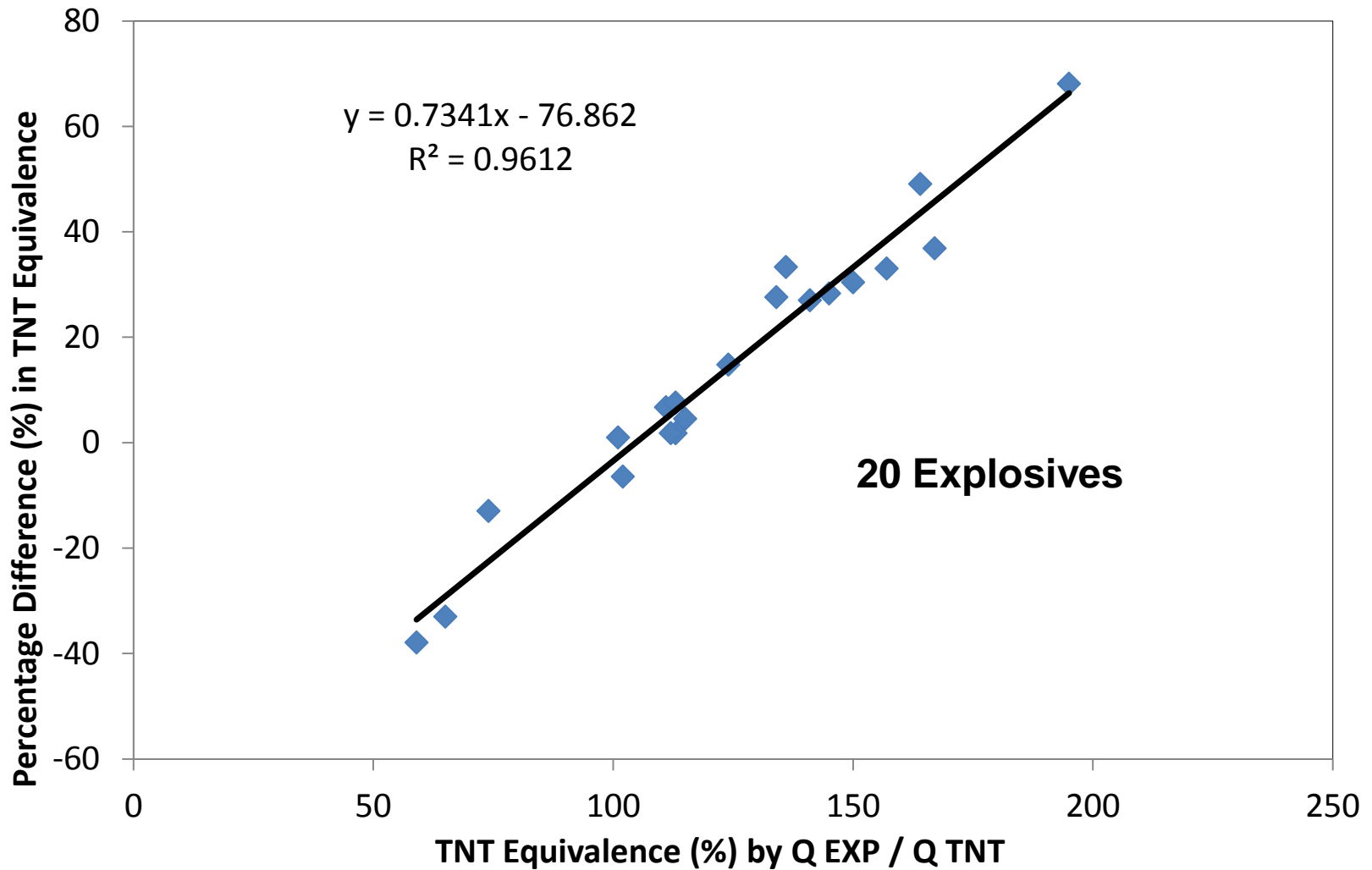


Figure 8. TNT Equivalence Difference for Heat (Q)

Line fit through origin

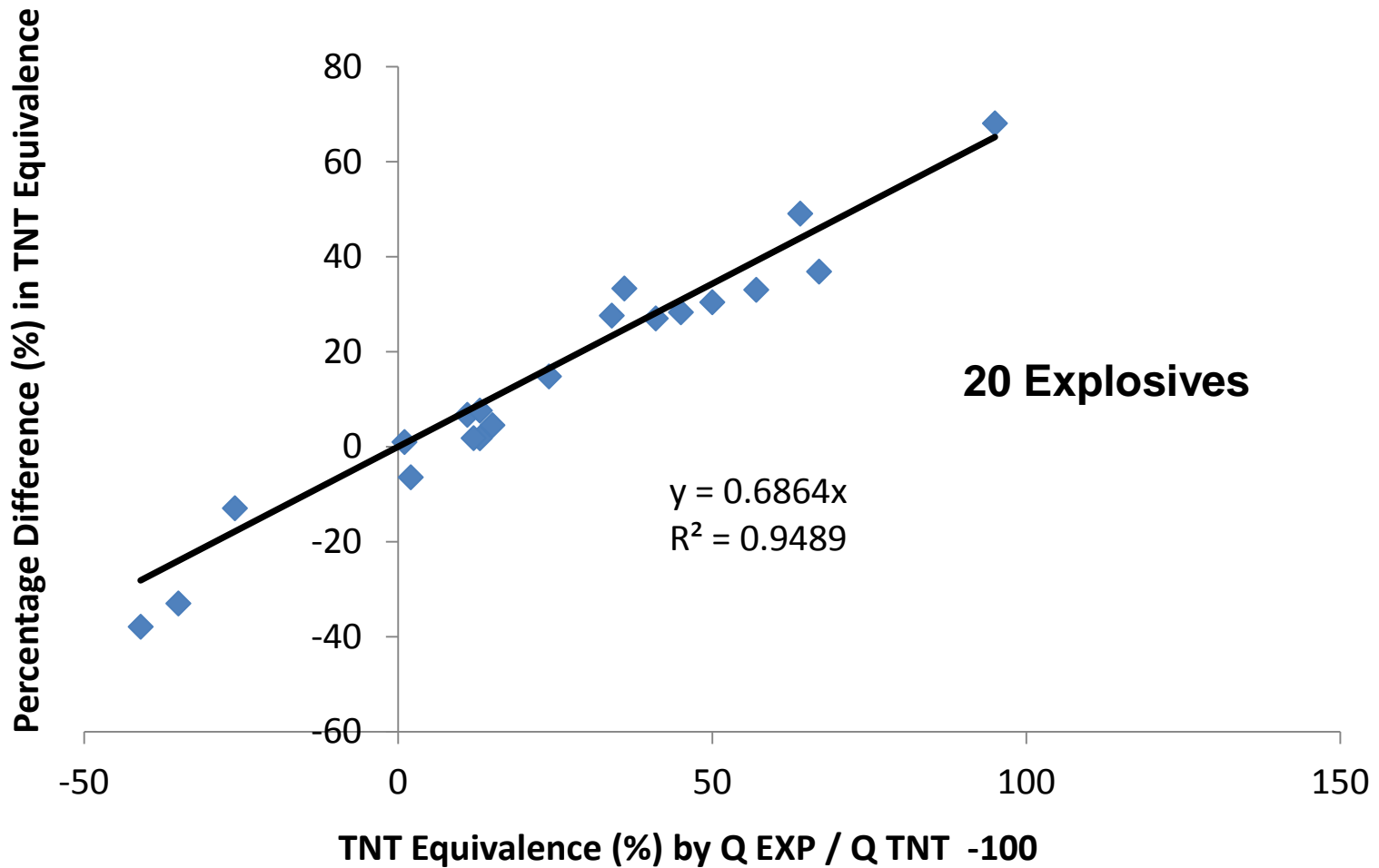


Table III. Some TNT Equivalence Comparisons by Percentage

Table III - has been updated and replaced by Table VI

Table IV. Comparison of Work TNT Equivalence Predictions

Explosive	Density (g/cc)	Heat of Detonation (MJ/kg)	CJ Pressure (GPa)	TNT Equivalence (%)				
				Expt	Calc from E	Difference, from E to Expt	Calc from PI	Difference, from PI to Expt
Non-Aluminised								
Ammon. Picrate	1.55	3.349	19.3	85	98	15.1	92	8.4
Amatol 60/40	1.50	2.638	13.3	95	69	-26.9	112	17.4
Amatol 50/50	1.55	2.931	16.4	97	84	-13.9	114	17.3
Comp A-3	1.59	4.605	27.5	109	136	25.1	141	29.5
Comp B	1.68	5.192	26.9	110	127	15.3	131	18.7
Comp C-3	1.60	6.071	24.5	105	121	15.0	135	28.7
Cyclotol 75/25	1.71	5.150	28.3	111	131	18.4	137	23.8
Cyclotol 70/30	1.73	5.066	29.1	110	134	21.4	135	22.5
Cyclotol 60/40	1.72	5.024	27.8	104	128	23.4	130	24.5
Ednatol 55/45	1.63	5.610	23.0	108	112	3.3	122	13.3
Pentolite 50/50	1.66	5.108	24.2	105	115	9.7	122	16.0
Picratol 52/48	1.63	4.564	20.8	100	101	0.6	103	3.3
PTX-1	1.64	6.364	25.2	111	121	9.3	123	10.7
PTX-2	1.70	6.531	28.8	113	134	18.6	133	17.5
Aluminised								
DBX	1.65	7.118	18.8	118	90	-23.7	143	21.3
HBX-3	1.81	8.834	22.3	116	98	-15.6	74	-36.3
MINOL-2	1.68	6.783	14.8	115	70	-39.2	145	25.7
MOX-2B	2.00	6.155	11.3	102	45	-55.8	49	-52.3
Torpex	1.81	7.536	26.1	122	115	-5.9	143	17.5
Tritonal	1.72	7.411	19.3	110	89	-18.8	120	9.1
Mean Absolute Difference						18.8		20.7

Figure 9. TNT Equivalence Difference comparison for Work

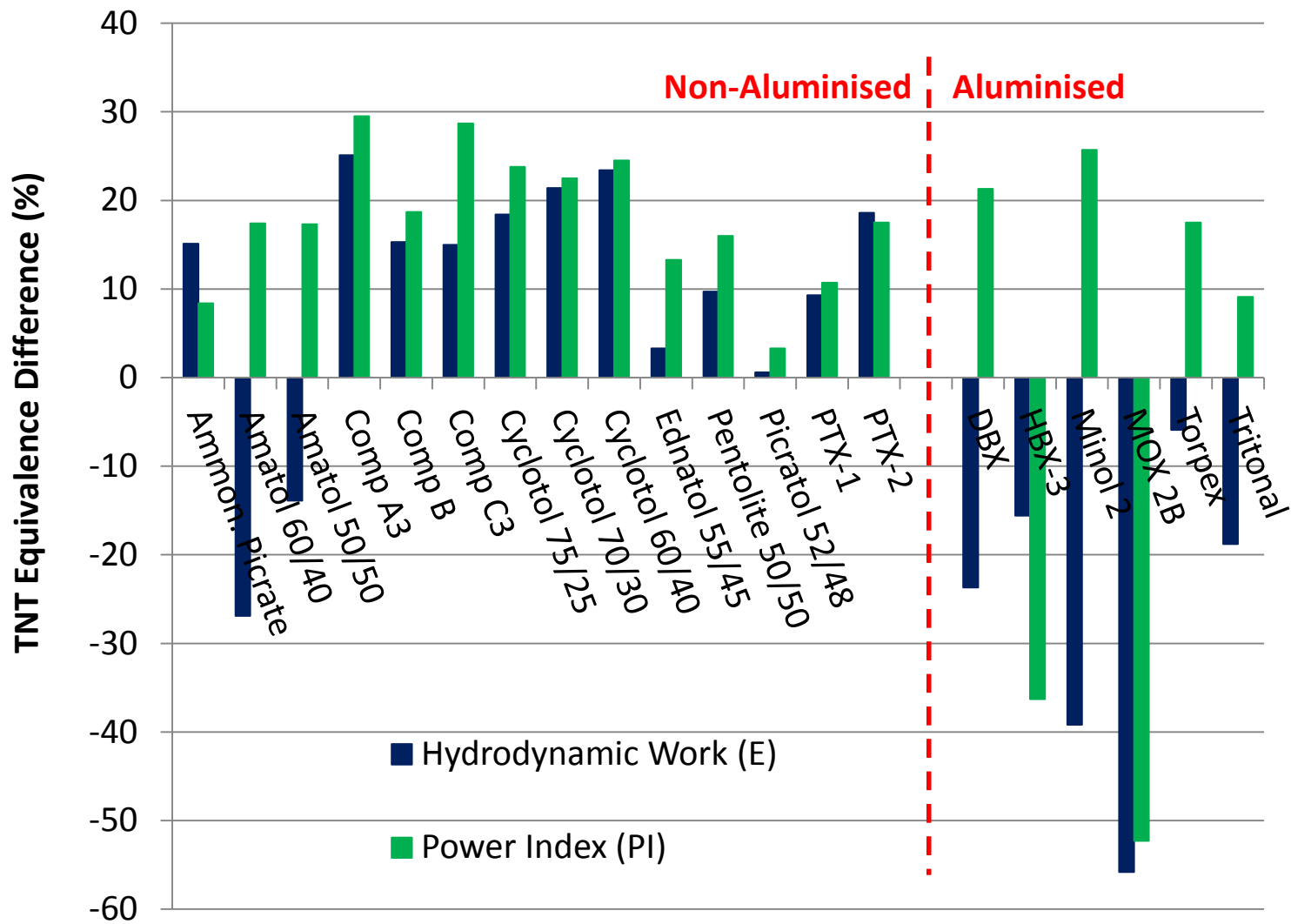


Table V. Comparison of Heat TNT Equivalence Predictions

Explosive	TNT Equivalence (%)				
	Expt	Standard Calc from Heat (Q)	Difference, from Standard Q to Expt	Updated Calc from Heat (Q)	Difference, from Updated Q to Expt
Non Aluminised					
Ammon. Picrate	85	74	-12.9	96	12.4
Amatol 60/40	95	59	-37.9	88	-6.9
Amatol 50/50	97	65	-33.0	92	-5.5
Comp A-3	109	102	-6.4	104	-4.6
Comp B	110	115	4.5	107	-2.8
Comp C-3	105	134	27.6	110	5.1
Cyclotol 75/25	111	113	1.8	107	-3.9
Cyclotol 70/30	110	112	1.8	106	-3.4
Cyclotol 60/40	104	111	6.7	106	2.0
Ednatol 55/45	108	124	14.8	109	0.6
Pentolite 50/50	105	113	7.6	107	1.4
Picratol 52/48	100	101	1.0	104	3.8
PTX-1	111	141	27.0	111	0.3
PTX-2	113	145	28.3	112	-1.0
Aluminised					
DBX	118	157	33.1	113	-3.8
HBX-3	116	195	68.1	117	1.1
MINOL-2	115	150	30.4	113	-2.1
MOX-2B	102	136	33.3	111	8.4
Torpex	122	167	36.9	115	-6.1
Tritonal	110	164	49.1	114	3.9
		Mean Absolute Difference	23.1		4.0

Figure 10. TNT Equivalence Difference comparison for Heat

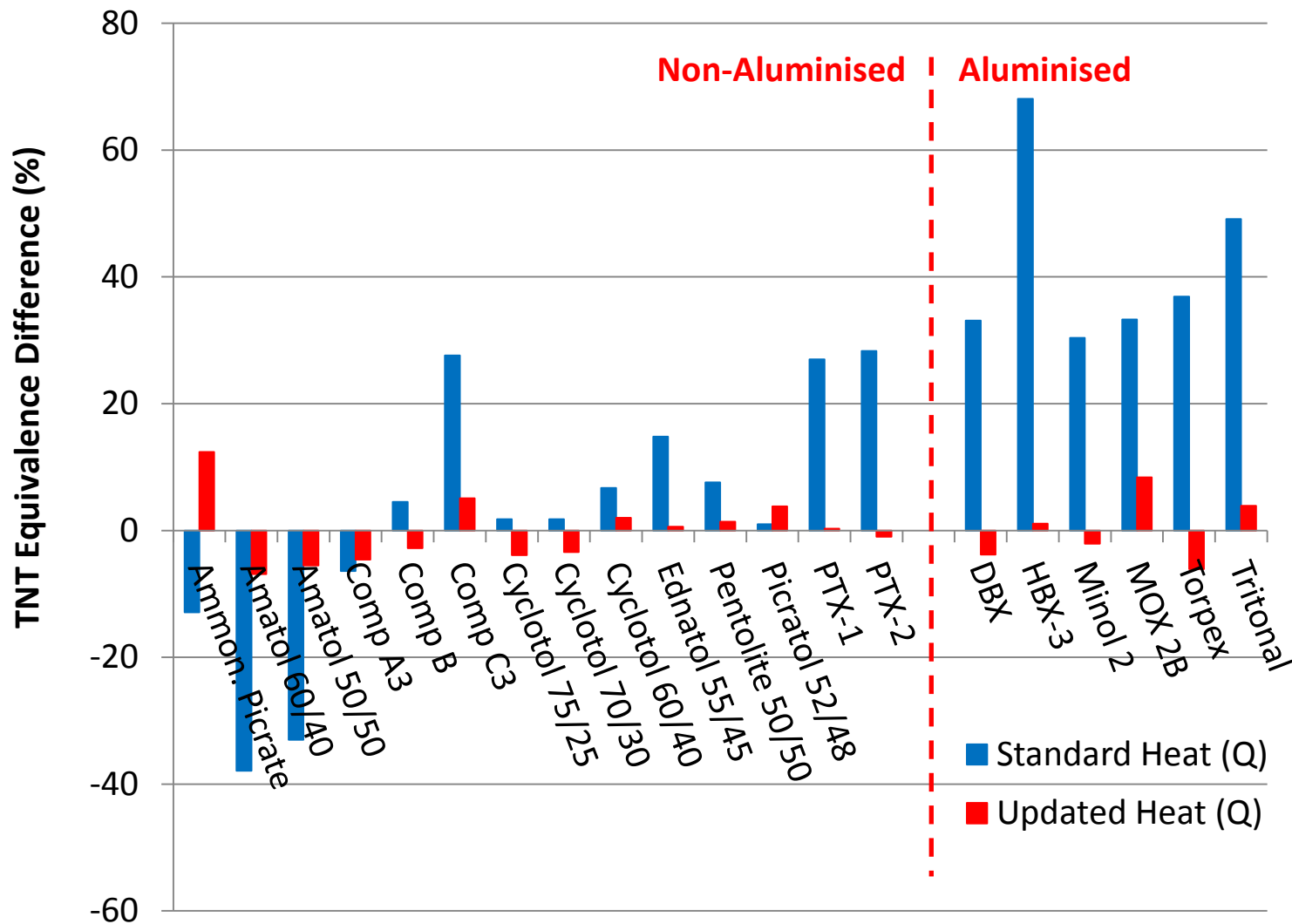


Table VI. TNT Equivalence Comparisons by Percentage

Explosive	From Expt	Berthelot Method	Difference Bethelot from Expt (%)	D^2 Method	Difference D^2 from Expt (%)
Non-Aluminised					
Ammon. Picrate	85	110	29.1	109	27.8
Amatol 60/40	95	138	45.6	137	43.8
Amatol 50/50	97	136	39.9	128	31.5
Comp A-3	109	168	54.5	136	24.5
Comp B	110	156	41.5	132	19.8
Comp C-3	105	161	53.5	132	26.1
Cyclotol 75/25	111	164	47.6	139	25.0
Cyclotol 70/30	110	161	46.1	136	23.4
Cyclotol 60/40	104	154	48.5	130	25.1
Ednatol 55/45	108	99	-7.9	67	-38.2
Pentolite 50/50	105	145	38.0	119	13.4
Picratol 52/48	100	115	14.5	105	4.5
PTX-1	111	147	32.0	123	10.8
PTX-2	113	158	40.1	133	17.4
Aluminised					
DBX	118	171	44.6	115	-2.7
HBX-3	116	90	-22.5	86	-26.0
MINOL-2	115	171	48.8	115	0.2
MOX-2B	102	58	-43.0	126	23.8
Torpex	122	171	40.1	110	-9.9
Tritonal	110	143	30.3	85	-22.5
Mean Absolute Difference			38.4		20.8

Figure 11. TNT Equivalence Difference for Berthelot and Cooper (D²)

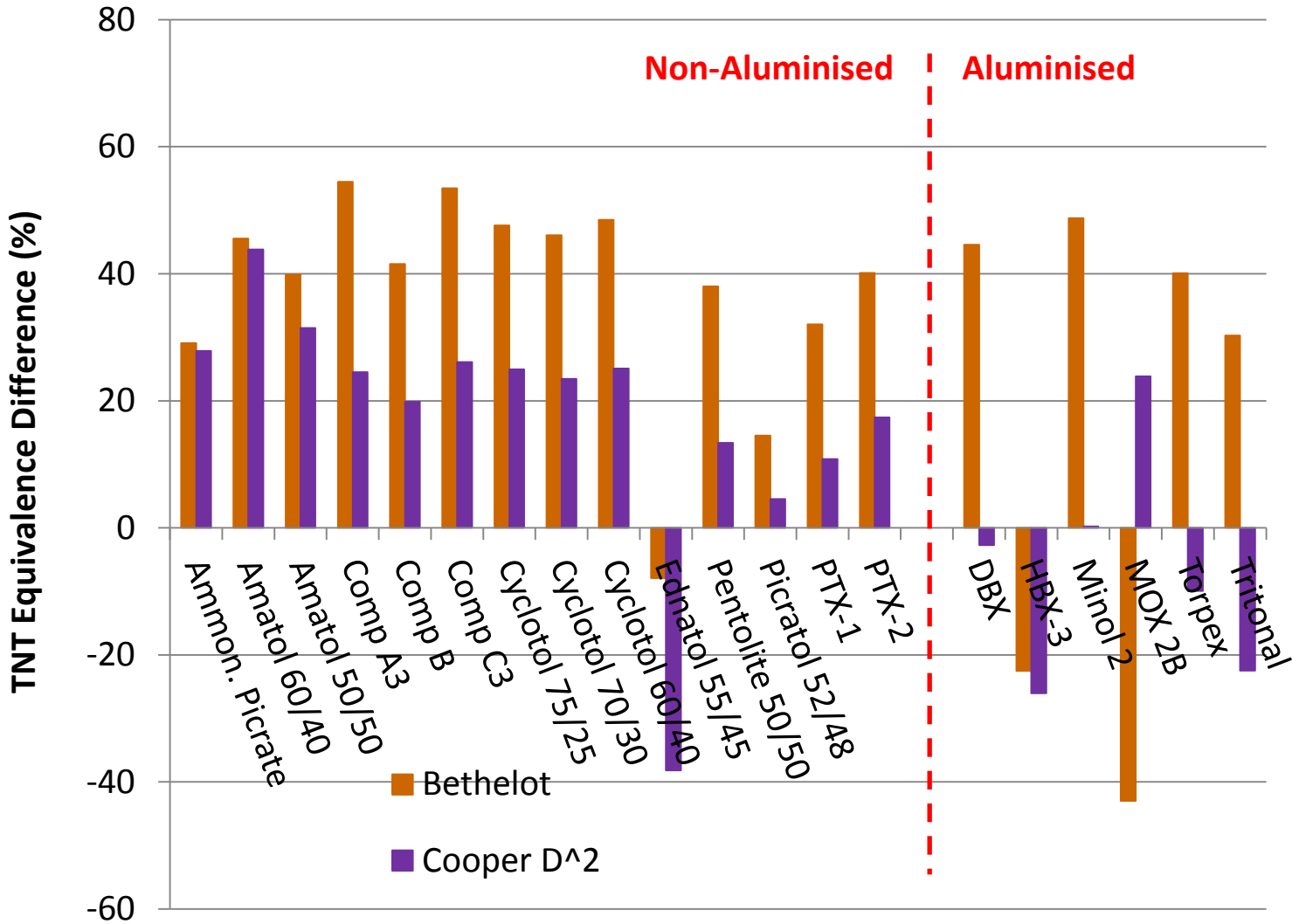


Table VII. Error Level Analysis of Methods

TNT Equivalence Difference (%) across the Methods

Method	Mean Absolute Difference	Standard Deviation	Maximum Absolute Difference	Ratio of Absolute Difference to Standard Deviation
Berthelot	38.4	26.3	54.5	2.1
D² (Cooper)	20.8	21.4	43.8	2.0
Hydrodynamic Work Function (E)	18.8	22.9	55.9	2.4
Power Index (PI)	20.7	20.5	52.3	2.6
Standard Heat (Q)	23.1	26.1	68.1	2.6
Updated Heat (Q)	4.0	5.0	12.4	2.5
Updated Heat (Q) with fit through point (100,0)	18.4	23.4	55.8	2.4

Ratios of 2 - 3 are typical for a Normal Distribution from a small sample

Conclusion

- A big problem with TNT Equivalence, typically 20% - 30% error
- Scaling Laws – they don't scale for Equivalence
- Five Theories have been detailed
- Theories compared to limited (open) trials data
- Power Index (PI) is the most reliable to date (21%)
 - Accounts for both Heat produced and Work available
- Recommended Standard Heat of Detonation (Q) is poor (26%)
 - But can be adjusted (Q update) to give the best of all fits (5%)

Any Questions ?

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