One Corps, One Regiment, One Team

Post-Tensioning Institute

Tri-Service Infrastructure Systems Conference

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Technical Revisions

- Corrosion Protection
- Partially Bonded Anchors
- Bond Length Design
- Bar Anchors
- Supplementary Requirements for Epoxy-Coated Strand Tendons
Rock Mass Shear Failure and References to PTI
Technical Revisions

Corrosion Protection

- Epoxy-Coated Bars
- Decision Tree *(Consequences Of Failure)*
- Corrugated
An epoxy-coated bar tendon grouted into a drill hole that has successfully passed the water pressure test is no longer considered Class I Protection.
Corrosion Protection
Epoxy Coated Bars

Epoxy coatings for bar and strand are not equivalent

- The average thickness required and possible on bars is only one third that of strand
- ASTM A775 and A934 allow an average of 3 holidays per lin. m of bar (without patching)
- ASTM A882 for strand allows only 2 holidays per 30 lin. m of stand (must be patched)
- The epoxy coating used on strand is more resistant to damage
Corrosion Protection Decision Tree
Corrosion Protection
Decision Tree

Consequences Of Failure

Third Edition
“If the failure of an isolated anchor could result in serious consequences, then the entire tendon length shall be protected by at least one layer of protection in addition to the grout or resin regardless of the aggressivity of the ground.”

Fourth Edition
“If the failure of the anchors could result in serious consequences, such as loss of life or serious economic impact, then the entire tendon length shall be protected by a Class I protection (See Section 5.3).”

Post-Tensioning Institute, Recommendations for Prestressed Rock and Soil Anchors, Fourth Edition
Corrosion Protection
Corrugated

‘Cutting of “windows” in the sheath or omission of the end cap in order to allow equalization of interior and exterior grout levels shall not be permitted.’

Post-Tensioning Institute, Recommendations for Prestressed Rock and Soil Anchors, Fourth Edition
Corrosion Protection

Corrugated

- HDPE Nominal thickness (0.060 in.)
- HDPE Minimum thickness (0.050 in.)

“A heavier wall thickness will be required for large diameter plastic tubing”

Post-Tensioning Institute, Recommendations for Prestressed Rock and Soil Anchors, Fourth Edition
Corrosion Protection

- Corrugated (Prinsco, Goldline)
  - 70-mil (measured at the crown)
    - 84-mil max
    - 56-mil minimum
  - 550 ft lengths
Corrosion Protection

Corrugated

- Critical buckling pressure for 10” diameter, 70-mil corrugated: 19 PSI
- Critical buckling pressure for 10” diameter, 100-mil corrugated: 39 PSI
“On projects where routine water pressure testing of the drill hole is specified, pressure testing of the encapsulation after installation and prior to any grouting should be considered”

Post-Tensioning Institute, Recommendations for Prestressed Rock and Soil Anchors, Fourth Edition
Corrosion Protection
Corrugated
Technical Revisions

Partially Bonded Anchors

What are they?
"Partially bonded free lengths provide redundant load transfer at the anchorage while at the same time leaving a certain amount of unbonded free length."

Post-Tensioning Institute, Recommendations for Prestressed Rock and Soil Anchors, Fourth Edition
Technical Revisions

Bond Length Design

Can we increase the efficiency?
Bond Length Design

“Extending the unbonded length of the prestressing steel a sufficient depth into the bond zone so that the bond length is partially loaded in compression”

Post-Tensioning Institute, Recommendations for Prestressed Rock and Soil Anchors, Fourth Edition
TYPICAL 49 TO 61 STRAND
NONRESTRESSABLE ANCHOR DETAIL

SCALE: 1" = 1'-0"
Bond Length Design

Over Grouting of the bare strand (5 to 10 feet)

- Eliminates disking of the grout near the top of the bond zone
- Compensates for small grout losses
- Allows for partially bonded anchors
Technical Revisions

Bars

Are they all created equal?
Bar Anchors

“For bars that have not been proof stretched during manufacturing to $0.8F_{pu}$, creep test data shall also be submitted”
Bar Anchors

- Threadbars up to a diameter of 1 3/8” are hot-rolled and then cold stretched (proof stretched)
  - Results in a very linear stress-strain curve to near the yield point
- Threadbars larger than 1 3/8” are cold drawn but not cold stretched
  - Because the drawing force used in the manufacturing process is much lower than the yield force the stress-strain curve is nonlinear
  - Results in:
    - Increased relaxation (ask for relaxation %)
    - Increased creep
    - Plastic behavior prior to yield
Bar Anchors

“The Creep Test is intended to determine the creep movement of the grout body through the ground at the test load.”

Post-Tensioning Institute, Recommendations for Prestressed Rock and Soil Anchors, Fourth Edition
Free Length
56.5 feet
Supplementary Requirements for Epoxy-Coated Strand Tendons

- Creep
- Relaxation
- Minimum free stressing length
Supplementary Requirements for Epoxy-Coated Strand Tendons

“Recent tests have shown that the amount of creep between strands from one manufacturer can vary by up to 50% from the average creep and between manufacturers by as much as a factor of 3.”

Post-Tensioning Institute, Recommendations for Prestressed Rock and Soil Anchors, Fourth Edition
<table>
<thead>
<tr>
<th>Test</th>
<th>Average % Creep After 10 Min</th>
<th>25 foot Free Length</th>
<th>50 foot Free Length</th>
<th>100 foot Free Length</th>
<th>150 foot Free Length</th>
</tr>
</thead>
<tbody>
<tr>
<td></td>
<td></td>
<td>elongation in Inches</td>
<td>elongation in Inches</td>
<td>elongation in Inches</td>
<td>elongation in Inches</td>
</tr>
<tr>
<td>M1 Bare Strand 16 Samples</td>
<td>0.0067%</td>
<td>0.017</td>
<td>0.034</td>
<td>0.063</td>
<td>0.102</td>
</tr>
<tr>
<td></td>
<td>MAX</td>
<td>0.0135%</td>
<td>0.030</td>
<td>0.060</td>
<td>0.120</td>
</tr>
<tr>
<td></td>
<td>Min</td>
<td>0.0012%</td>
<td>0.004</td>
<td>0.007</td>
<td>0.015</td>
</tr>
<tr>
<td></td>
<td>STDEV</td>
<td>0.0028%</td>
<td>0.008</td>
<td>0.017</td>
<td>0.034</td>
</tr>
<tr>
<td>M1 Epoxy Strand 21 Samples</td>
<td>0.0032%</td>
<td>0.029</td>
<td>0.055</td>
<td>0.110</td>
<td>0.185</td>
</tr>
<tr>
<td></td>
<td>MAX</td>
<td>0.0171%</td>
<td>0.051</td>
<td>0.103</td>
<td>0.205</td>
</tr>
<tr>
<td></td>
<td>Min</td>
<td>0.0042%</td>
<td>0.013</td>
<td>0.025</td>
<td>0.050</td>
</tr>
<tr>
<td></td>
<td>STDEV</td>
<td>0.0034%</td>
<td>0.010</td>
<td>0.020</td>
<td>0.040</td>
</tr>
<tr>
<td>M2 Bare Strand 4 Samples</td>
<td>0.0067%</td>
<td>0.030</td>
<td>0.040</td>
<td>0.080</td>
<td>0.120</td>
</tr>
<tr>
<td></td>
<td>MAX</td>
<td>0.0103%</td>
<td>0.030</td>
<td>0.080</td>
<td>0.120</td>
</tr>
<tr>
<td></td>
<td>Min</td>
<td>0.0050%</td>
<td>0.015</td>
<td>0.030</td>
<td>0.060</td>
</tr>
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<td></td>
<td>STDEV</td>
<td>0.0023%</td>
<td>0.007</td>
<td>0.014</td>
<td>0.027</td>
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<td>M2 Epoxy Strand 26 Samples</td>
<td>0.0248%</td>
<td>0.074</td>
<td>0.149</td>
<td>0.297</td>
<td>0.446</td>
</tr>
<tr>
<td></td>
<td>MAX</td>
<td>0.0421%</td>
<td>0.126</td>
<td>0.255</td>
<td>0.505</td>
</tr>
<tr>
<td></td>
<td>Min</td>
<td>0.0163%</td>
<td>0.049</td>
<td>0.096</td>
<td>0.195</td>
</tr>
<tr>
<td></td>
<td>STDEV</td>
<td>0.0067%</td>
<td>0.020</td>
<td>0.040</td>
<td>0.081</td>
</tr>
</tbody>
</table>

Note: Those samples tested to 70% were not included.
Supplementary Requirements for Epoxy-Coated Strand Tendons

<table>
<thead>
<tr>
<th>OPTIONS</th>
<th>DESIGN LOAD ($F_{pu}$)</th>
<th>CREEP CRITERIA</th>
<th>TEST LOAD as % of $F_{pu}$</th>
<th>COMMENTS</th>
</tr>
</thead>
<tbody>
<tr>
<td>1 Test to 1.5 DL</td>
<td>0.53</td>
<td>None</td>
<td>80</td>
<td>No Creep Test is conducted</td>
</tr>
<tr>
<td>2 Test to 1.33 DL</td>
<td>0.53</td>
<td>Same as bare strand</td>
<td>70</td>
<td>Limited test data suggest creep for epoxy-coated strand at this stress level is similar to bare strand</td>
</tr>
<tr>
<td>3 Test to 1.33 DL and conduct subsequent Lift-off Tests</td>
<td>0.60</td>
<td>None</td>
<td>80</td>
<td>Lift-off must be at least the original load minus the predicted tendon relaxation</td>
</tr>
</tbody>
</table>
Supplementary Requirements for Epoxy-Coated Strand Tendons

“In defining the design load, the higher relaxation in epoxy-coated strand should be considered. The relaxation of epoxy-coated strand can be as high as 6.5% in 1,000 hours at $0.7F_{pu}$, compared to 2.5% for bare strand.

Both creep and relaxation are the results of plastic deformation in the strand under load.”

Post-Tensioning Institute, Recommendations for Prestressed Rock and Soil Anchors, Fourth Edition
Supplementary Requirements for Epoxy-Coated Strand Tendons

“A longer free stressing length is required for epoxy-coated strand to compensate for higher wedge seating loss, typically 15 to 25 mm (5/8 to 1 in.), versus 3 to 12 mm (1/8 to 3/8 in) for bare strand.”

Post-Tensioning Institute, Recommendations for Prestressed Rock and Soil Anchors, Fourth Edition
Rock Mass Shear Failure and References to PTI
(3) Rock-mass shear failure

(a) Tensioned structural anchors. With all tensioned structural-anchor systems, a major consideration is determining how deep to install the anchors. An anchor system that is too shallow may cause tension and cracking to occur along potential failure planes in the foundation, and a system too deep is uneconomical. PTI recommends normal bond length not less than 3.0m (10ft) for bars and 4.5m (15ft) for strand. Bond lengths greater than 10m (35ft) are normally not used. PTI recommends free stressing lengths to be at least 3.0m (10ft) for bar tendons and 4.5m (15ft) for strand tendons. Center-to-center spacings between anchors shall be at least 1.5m (5ft) unless unusual circumstances dictate. The fixed end (dead end) anchorages should be staggered.
Post-Tensioning Institute, “Recommendations for Prestressed Rock and Soil Anchors”, does not give guidance on determining how deep to install the anchors.
“When selecting the elevation of the top of the bond length, the designer must consider the resistance to pullout of the rock mass, which also governs anchor length.” PTI
Anchor Depth Design

“The anchor depth is taken as the anchor length necessary to develop the anchor force required for stability.”  EM 1110-1-2908
One Corps, One Regiment, One Team

US Army Corps of Engineers
Huntington District

STRESSING LENGTH

- 60° - 90° CONE
Anchor Depth Design

EM 1110-1-2908 gives 2 formulas for competent rock:
1. Single Anchor in Competent Rock
2. Single Row of Anchors in Competent Rock
EM 1110-1-2908 gives 3 formulas for fractured rock:

1. Single Anchor in Fractured Rock
2. Single Row of Anchors in Fractured Rock
3. Multiple Row of Anchors in Competent or Fractured Rock
2 - 61 Strand Anchors @ 5.96° from Top of Dam

10 - 54 Strand Anchors @ 45° from Downstream Face of Dam

Approximate Location of Fault Zone

Interbedded Orthoquartzite & Shale

Thrust Block

Lean Concrete Fill

Ebris and Shale

Lean Concrete Fill

Interbedded Orthoquartzite & Shale

10 - 54 Strand Anchors @ 45° from Downstream Face of Dam

Approximate Location of Fault Zone

Interbedded Orthoquartzite & Shale

Thrust Block

Lean Concrete Fill

Ebris and Shale
Multiple rows of anchors in competent rock, with a factor of safety of 1.5

\[
\frac{(FS \cdot F)}{yls} = \text{Suggested depth of anchor for overall cone stability}
\]

360 feet
single anchor in fractured rock with the combined
design load of all the anchors in that area

\[
\text{cbrt}\left(\frac{3FS^2F}{w^3.14159}\right) \quad 65.3 \text{ feet}
\]

\text{19,008,000 pounds of anchor force}
One Corps, One Regiment, One Team

US Army Corps of Engineers
Huntington District

M-18

CL

2+00 N 3+00 N 4+00 N 5+00 N

1+00 N
3-D CADD Drawing of Anchor Failure Cones Mon-18
The buoyant weight of the rock mass engaged by the anchors in monolith 18 is 3.75 times that needed to resist the total force of the anchors.
Questions ?

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