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#### SEISMIC REMEDIATION OF THE CLEMSON UPPER AND LOWER DIVERSION DAMS; DEEP SOIL MIX CONSTRUCTION

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## **Bids**

| _                      | Total Bid<br>mary | Production Soil Cement<br>Bid Summary |                         |  |  |  |
|------------------------|-------------------|---------------------------------------|-------------------------|--|--|--|
| Government<br>Estimate | \$7,768,587       | Winning Bid                           | \$107/yard <sup>3</sup> |  |  |  |
| Winning &<br>Low Bid   | \$7,744,657       | Low Bid                               | \$70/yard <sup>3</sup>  |  |  |  |
| High Bid               | \$12,592,400      | High Bid                              | \$199/yard <sup>3</sup> |  |  |  |
| Average                | \$9,248,526       | Average                               | \$126/yard <sup>3</sup> |  |  |  |

Winning Bid: RAITO Inc. of Crofton, Maryland



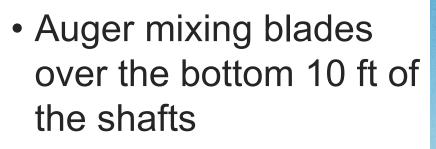
#### **Bids**

| <b>Additional Soil Cement Bid Summary</b> |                         |  |  |  |  |  |
|---|-------------------------|--|--|--|--|--|
| Winning & Low Bid                         | \$220/yard <sup>3</sup> |  |  |  |  |  |
| High Bid                                  | \$819/yard <sup>3</sup> |  |  |  |  |  |
| Average                                   | \$556/yard <sup>3</sup> |  |  |  |  |  |

- Large track mounted rig
- Six in-line, 3-footdiameter, ~50-foot-long soil mix augers
- Four electrical motors drive the augers at either 20 or 40 rpms



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- Overlap adjacent mixing columns by 1 ft
- Average wall width of 2.76 feet
- Adjacent augers
   vertically offset by 1 ft



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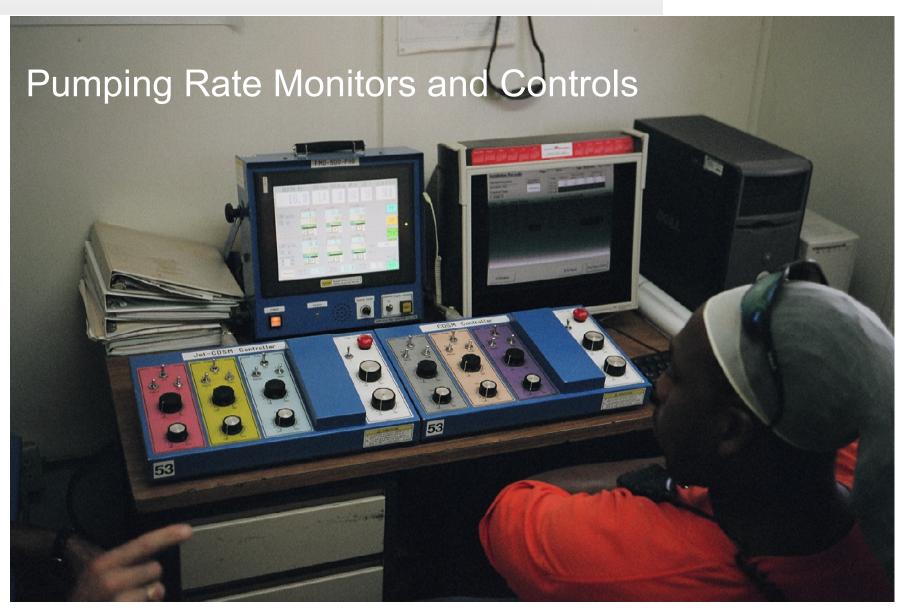
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Tanker truck off-loading cement

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#### **Flow Meters**

#### Pump



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Monitored Parameters:

- Depth
- Time Injected Cement / Foot

Resistance

- Flow Rate
- Cable Load
- Electrical Motor Load
- Verticality

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#### **Typical Installation Record**

#### Installation Records

#### Project Name: Clemson

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Element # : UDSW40196

Rig # : 1

7 / 28 / 2004

PAGE 1

| Mixing System | Depth | Slurry Injection | Speed (ft/min) |      |      |
|---------------|-------|------------------|----------------|------|------|
| Design Data   | (ft)  | Down             | Up             | Down | Up   |
| 1st Layer     | 8.5   | 1.0              | 0.0            | 40.0 | 40.0 |
| 2nd Layer     | 50.0  | 17.6             | 0.0            | 3.5  | 5.5  |
| 3rd Layer     |       |                  |                |      |      |
| 4th Layer     |       |                  |                |      |      |

|     | Depth | Time    | Speed    | Rotation |         | Slurry Injection Volume (gal) |         |         |         |                             | Energy |   |
|-----|-------|---------|----------|----------|---------|-------------------------------|---------|---------|---------|-----------------------------|--------|---|
|     | (ft)  | (mm:ss) | (ft/min) | (rpm)    | Columnl | Column2                       | Column3 | Column4 | Column5 | Column6                     | Index  |   |
|     | 0.0   | 0:00    |          |          |         |                               |         |         |         |                             |        |   |
|     | 3.0   | 0:25    | 7.2      | 19       | 9.8     | 7.1                           | 7.2     | 8.4     | 7.4     | 7.5                         | 39     |   |
|     | 6.0   | 1:58    | 1.5      | 19       | 21.3    | 22.7                          | 20.7    | 21.8    | 22.3    | 22.6                        | 222    |   |
|     | 8.5   | 3:50    | 0.6      | 17       | 78.0    | 73.1                          | 73.5    | 74.3    | 71.1    | 74.3                        | 805    |   |
|     | 9.0   | 0:24    | 1.2      | 19       | 17.6    | 18.3                          | 18.3    | 18.1    | 18.5    | 18.3                        | 377    |   |
|     | 12.0  | 1:27    | 2.0      | 19       | 54.6    | 54.4                          | 54.3    | 54.4    | 54.5    | 54.3                        | 198    |   |
|     | 15.0  | 1:27    | 2.0      | 19       | 52,0    | 52.3                          | 52.2    | 52.1    | 52.2    | 52.3                        | 194    |   |
| Î   | 18.0  | 1:13    | 2.4      | 19       | 58.6    | 58.3                          | 57.3    | 58.4    | 58.0    | 58.1                        | 144    |   |
|     | 21.0  | 1:08    | 2.6      | 19       | 64.6    | 64.4                          | 63.2    | 64.5    | 64.5    | 64.4                        | 76     |   |
| ľ   | 24.0  | 0:56    | 3.2      | 38       | 53.5    | 53.4                          | 55.2    | 53.3    | 53.4    | 53.4                        | 40     |   |
|     | 27.0  | 1:37    | 1.8      | 40       | 57.1    | 58.6                          | 58.7    | 58.6    | 58.1    | 57.3                        | 110    |   |
|     | 30.0  | 1:04    | 2.8      | 40       | 59.6    | 54.3                          | 56.0    | 53.7    | 56.6    | 57.4                        | 35     |   |
|     | 33.0  | 1:05    | 2.7      | 40       | 56.5    | 56.6                          | 57.3    | 54.9    | 57.1    | 56.9                        | 36     |   |
| a.0 | 36.0  | 3:00    | 1.0      | 39       | 56.9    | 59.8                          | 61,0    | 60.6    | 60,6    | 62.3                        | 275    |   |
| -   | 39.0  | 1:30    | 2.0      | 21       | 81.3    | 75.5                          | 81.2    | 79.5    | 81.2    | 82.0                        | 84     | · .   |
| T   | 42.0  | 0:57    | 3.1      | 19       | 53.7    | 53.8                          | 53.9    | 53.8    | 53.9    | 53.8                        | 96     | e de la companya de l<br>La companya de la comp |
| 1   | 45.0  | 2:14    | 1.3      | 19       | 62.7    | 63.5                          | 63.6    | 63.1    | 64.1    | 63.8                        | 348    |   |
|     | 47.0  | 3:58    | 0.5      | 19       | 111.4   | 110.4                         | 112.3   | 40.6    | 39.6    | 40.2                        | 1069   | ***   |
| -   | 47.1  | 1:31    | 0.0      | 19       | 33.9    | 34.2                          | 34.2    | 32.4    | 32.8    | 30.9                        | 1337   |   |
| -   | 18 0  | 0.31    | 10       | 10       | 0 5     | 0.5                           | 0.5     | 0.5     | 0.5     | and the second day when the |        | **  |





## Construction – Planned QA/QC



#### QA/QC – Wet Grab Soil-Cement Samples Frequency:

- Two sets of samples per wall
- Not less than one set per work shift per rig

Set: Consists of 4 samples each at top, middle, bottom depths

Procedure:

- Screen samples on 1-inch sieve
- Cut particles retained to just pass the 1-inch sieve and then to be remixed with sample
- Collect enough soil-cement per sample to make four full cylinders (6-inch diameter by 12-inch height)

Unconfined tests: @ 7 days, 28 days(2), and 56 days; (12 @ 28)

## Construction – Planned QA/QC



#### **QA/QC - Core Samples**

Where:

- Two locations per test section (Test section was a single wall)
- Two locations within any production wall where wet grab samples do not meet strength criteria
- <u>When:</u> Only after strength from unconfined tests on wet grab cylinders indicate that soil-cement strength is unsuitable
- <u>Type of core</u>: Continuous, double tube or triple tube, minimum 3inch diameter

<u>Supplemental coring:</u> If recovery less than 85 % in any run <u>Testing:</u> Unconfined compression on six samples per boring



#### **Test Sections**

#### Two test sections per dam.

Establish **base procedures** for installation of production walls.

- If **f'sc < criteria**, then:
- use smaller S, wall spacing, that will meet criterion or

• Contractor may **modify procedures** (e.g. higher cement ratio) during production to increase f'sc.

#### Construction – Planned QA/QC



#### QA/QC – Soil-Cement Strength Criteria

Average 28-day compressive strength for each wall:

• Average f'sc (28 day) =/> 77.4 psi x (S / Wa)

Average of all samples (12) from six wet grab locations or all samples (12) from two core borings (when wet grab samples fail)

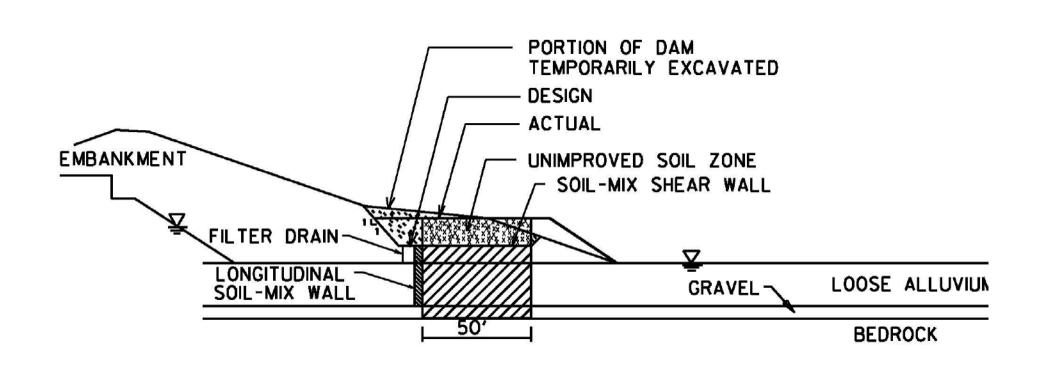
• One sample per wall may have f'sc < 2/3 criterion</p>





#### **Construction-Excavation of Berm**

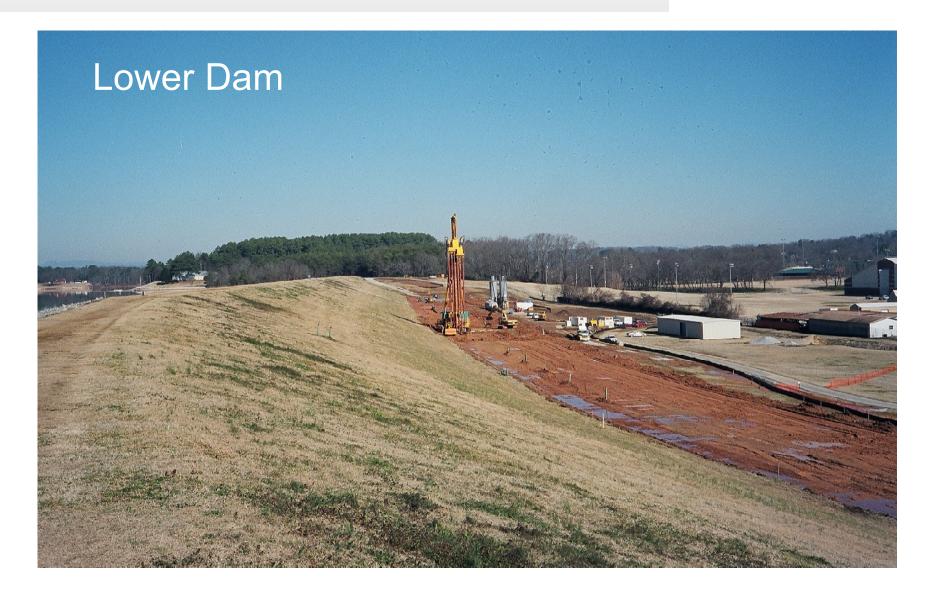




**Design vs Actual – Schematic Section** 

#### **Construction-Excavation of Berm**

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Sampler plugged with soil from unimproved zone

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Attempts at Wet-Grab Sampling (Unsuccessful)



## Coring Rig for Soil-Cement Sampling











#### Core in core box; note plastic sheath and burlap





Logging of core and selecting test specimens

#### Construction – Actual QA/QC



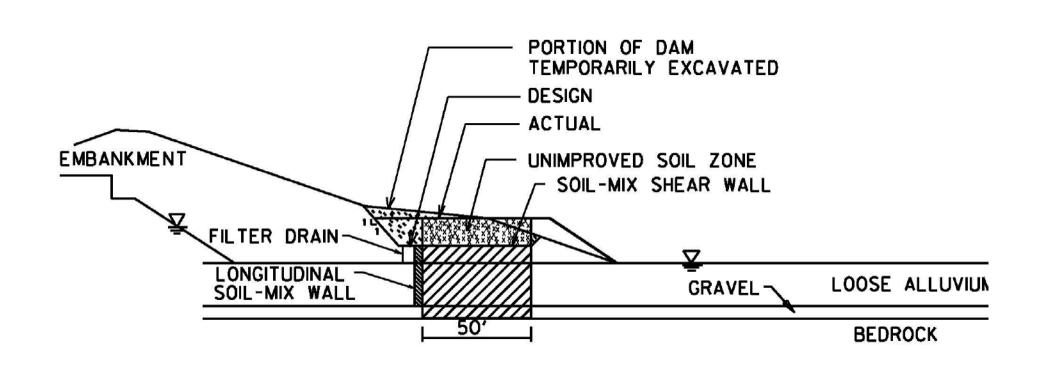
#### QA/QC – Soil-Cement Strength Criteria

Average 28-day compressive strength for each wall:
Average f'sc (28 day) =/> 77.4 psi x (S / Wa)
Average of all samples (12) from six wet grab locations or all samples (12) from two core borings (when wet grab samples fail)

- One sample per wall may have f'sc < 2/3 criterion</p>
- Criteria evolved to single core boring for a day's production; minimum six samples per core; one sample may have f'sc < 2/3 average; additional core borings as required

#### **Construction-Excavation of Berm**





**Design vs Actual – Schematic Section** 

## **Construction-Drain Construction**

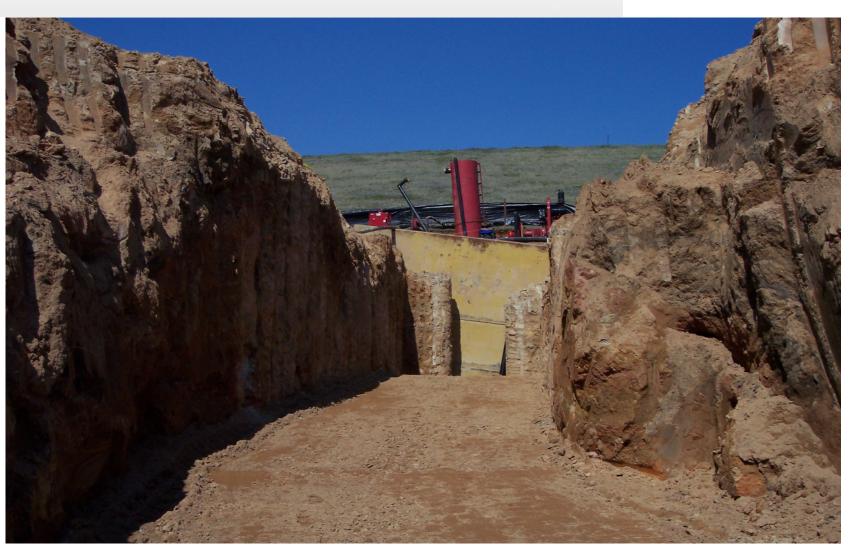
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#### Trench box and dewatering pump station

## Construction-Drain Construction

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#### Installation of discharge line; note slot in longitudinal wall

## **Construction-Drain Construction**

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#### Cleanouts on drain line



## Construction – Soil-Cement Production Mixes



**Cement Injection Rates:** 

- 840 lb/yd<sup>3</sup> (500 kg/m<sup>3</sup>) at start
- 670 lb/yd<sup>3</sup> (400 kg/m<sup>3</sup>) at end

Water-Cement Ratio: 0.6 to 0.7

## Construction – Penetration "Refusal" Criteria



- Advancement Rate < 0.2 foot/minute</li>
- Cable load < one ton</li>
- Duration > one minute

## Construction- Problems and Remedies



# **Problems:**

- Zones where f'sc of soil cement did not meet criteria, probably due to organic content and/or low pH, in ~13% of walls
- Difficult to judge and achieve penetration into dense strata, in ~20% of walls

## Remedy:

Additional elements or walls

#### Construction – Lessons



- Expect zones of significant deviation of f'sc (allow some random deviations, correct deviation trends or patterns)
- Cover as large a range of soils as possible in design mix testing
- Test soil samples for pH and organic content
- Use **coring** and not wet grab sampling for QA
- Use recovery and core RQD or continuity as part of the QA criteria

#### Construction – Lessons



- Include a defined number of additional soil borings and core borings as part of the construction program
- Define required remedial actions if f'sc is low or if penetration is not achieved
- Require use of computerized data collection and injection control for QC

## Summary – Design & Construction



The use of soil mix shear walls to provide reinforcing of the loose soil against seismic deformations and liquefaction shear slides at the Clemson Dams was feasible and cost effective



#### **Clemson Diversion Dams**







Clemson University can continue to safely perform Football Rituals in Death Valley.