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Effect of Yaw and Obliquity on Penetration

 High velocity kinetic energy long rods are one of the most important munitions of the main battle tank.



- One way to protect a tank against a kinetic energy long rod is to configure a series of thin plates as passive armor.
- These plates are generally oblique.
- This target is capable of breaking the rod.



Effect of Yaw and Obliquity on Penetration

- The penetration process of a rod while penetrating a thin and oblique target is characterized by the following factors:
 - erosion at the nose of the rod (large plastic strain)
 - rotation and bending of the rod
 - long rod breakage
 - interaction between the broken parts and the target
- Yaw worsens the above phenomena



The goals of the present work

- To build a numerical simulation of the penetration process.
- Validation of the numerical model with experimental results.
- Using the model to study the influence of the initial yaw on projectile penetrability.
- Using the numerical model to design an improved projectile.



Obliquity is the angle between the velocity vector of the rod and the normal to the target.





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Yaw is the angle between the velocity vector direction of the rod and it's axis of symmetry.



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Negative initial yaw angle

Positive initial yaw angle



Zero initial yaw angle



EXPERIMENTS



Schematic of the Experimental Set-up

The tungsten-alloy long rod penetrates the thin steel target











Experimental Results

It is apparent that:

- the rod was bent and its nose was broken
- for a negative initial yaw angle the rod bends up
- for a positive initial yaw the rod bends down
- for a zero initial yaw the bending is minimal





NUMERICAL SIMULATION





A three-dimensional time-dependent finite element numerical simulation (MSC/DYTRAN) was performed in order to emulate the penetration process of the rod during and after target penetration .



Numerical Simulation

- Lagrangian explicit model.
- adaptive contacts to model the rod target interaction
- a nonlinear, plastic material description with isotropic hardening:

$$\boldsymbol{s}_{y} = \boldsymbol{s}_{0} + \frac{E E_{h}}{E - E_{h}} \boldsymbol{e}_{p}$$

• a polynomial equation of state:

 s_0 E_h e

$$p = \begin{cases} a_1 \mathbf{m} + a_2 \mathbf{m}^2 + a_3 \mathbf{m}^3 + (b_0 + b_1 \mathbf{m} + b_2 \mathbf{m}^2 + b_3 \mathbf{m}^3) \mathbf{r}_0 e & \mathbf{m} > 0 \\ a_1 \mathbf{m} + (b_0 + b_1 \mathbf{m}) \mathbf{r}_0 e & \mathbf{m} \le 0 \end{cases}, \mathbf{m} = \frac{\mathbf{r}}{\mathbf{r}_0} - 1$$



- A failure criterion model in the form of a user written subroutine was added to the MSC/DYTRAN code:
- it depends upon the state of the material in the element (stress, strain, pressure ...)
- it is based on two types of material failure:
 - erosion failure
 - static maximum plastic strain failure











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Numerical Simulation

The bending process:

- enlarges the hole crater in the target
- decreases the rod velocity
- diverts the direction of the penetrator
- In addition, for none zero initial yaw values:
- the side of the rod pointing in the direction of its velocity is damaged. (This side is in greater contact with the target because of the velocity direction).



- The overall results are a weakening of the rod and a decrease in its ability to penetrate a series of plates following the original thin plate target.
- For large yaw angles the bending of the long rod will cause it to break into several pieces.